

where  $G(s) = C(sI - A)^{-1}B$ ,

$$M(s) = K(sI - (A - HC))^{-1}B$$

$$N(s) = K(sI - (A - HC))^{-1}H$$

In the usual discussion of state-space theory of observer-controller design, we make the following assumptions:

$[A, B, C]$  is a minimal triple that realises  $G(s)$ ;

$K$  is such that  $(A - BK)$  has spectrum  $\subseteq \mathbb{C}^-$ ;

$H$  is such that  $(A - HC)$  has spectrum  $\subseteq \mathbb{C}^-$ ;

then, the compensator consisting of  $M$ ,  $N$  and the unity feedback of  $\Xi$  is itself stable. Choice of spectrum of  $A - HC$  governs how ~~fast~~ fast  $\hat{x}(t)$  converges to  $x(t)$ , Choice of spectrum of  $A - BK$  is a ~~not~~ specification of

the closed loop system behavior.

It is desirable to carry out the whole design process in the frequency domain, skipping the stage of state space realization and finding  $K$  and  $H$ . We do this below, using Figure 3 as a guide.

$$Y(s) = G(s) u(s)$$

$$u(s) = V(s) - \Xi(s)$$

$$\Xi(s) = M(s) u(s) + N(s) Y(s)$$

SISO assumption  $\left\{ \begin{array}{l} \text{From here-on we consider the} \\ \text{single-input single-output (SISO)} \\ \text{case only, allowing easier algebra.} \\ \text{In that case,} \end{array} \right.$

$$Y(s) = \frac{G(s)}{1 + M(s) + N(s)G(s)} V(s)$$

define the closed loop transfer function

$$G_c(s) = \frac{G(s)}{1 + M(s) + N(s)G(s)}$$

Let  $G(s) = b(s)/a(s)$ , as before,  
 $M(s) = m_u(s)/m_d(s)$  and,  
 $N(s) = n_u(s)/n_d(s)$ , where  
 all transfer functions are rational  
 strict, proper and reduced (i.e. free of  
 common factors in the numerator -  
 denominator expressions).

Also  $a, m_d, n_d$  are monic.  
 Then, the closed loop transfer function

$$G_c(s) = \frac{b/a}{1 + \frac{m_u}{m_d} + \frac{n_u}{n_d} \frac{b}{a}}$$

$$= \frac{b n_d a}{m_d n_d a + m_u n_d a + n_u m_d b}$$

Suppose there exist  $m_d, m_u, n_d, n_u$

such that

\*

$$m_u n_d a + n_u m_d b = m_d n_d m$$

for a specified polynomial  $m(s)$   
 $\deg(m(s)) \leq n-1$ .

Then, clearly, canceling  $m_d n_d$  from the numerator and denominator, we obtain,

$$G_c = \frac{b}{a + m}$$

Specifying  $m$  and solving (\*) yields any closed loop poles we might want — i.e.  $m(s)$  is a design specification.

Solving (\*) is equivalent to solving

$$(**) \quad \frac{m_u}{m_d} a + \frac{n_u}{n_d} b = m$$

$$\left( \Leftrightarrow M a + N b = m \right)$$

for strictly proper transfer functions  $M, N$ .

We solve (\*\*) in three steps.

- ① Find  $x(s), y(s)$   $\deg(x) < \deg(b)$   
 $\deg(y) < \deg(a)$  such that  
 $x(s)a(s) + y(s)b(s) \equiv 1$ .

This is the BEZOUT step.

(2) select monic polynomial  $S(s)$  with  $\deg(S) = n$ .

$$\text{Define } f = x m S$$

$$g = y m S$$

then

$$\frac{f}{S} a + \frac{g}{S} b = (x a + y b) m$$
$$= m$$

Thus  $\frac{f}{S}$  and  $\frac{g}{S}$  solve (\*\*)

but fail to meet the strict properness conditions. In fact they are polynomials and not rational functions. We remedy this in the next step.

(3) Divide  $g$  by  $a$  to get

$$g = l a + g_0$$

$$\deg(g_0) < \deg(a) = n$$

$$\text{Define } f_0 = f + l b$$

$$\text{Then } M = \frac{f_0}{\delta}, \quad N = \frac{g_0}{\delta}$$

solve (\*\*), and respect the strict proper rationality conditions.

proof :

$$\begin{aligned} & M a + N b \\ &= \frac{(f_0 a + g_0 b)}{\delta} \\ &= \frac{(f + lb) a + (g - la) b}{\delta} \\ &= \frac{f a + g b}{\delta} \\ &= \frac{(x a + y b) m \delta}{\delta} \\ &= m \end{aligned}$$

$$\deg(f_0 a) = \deg(m \delta - g_0 b)$$

$$\deg(f_0) = \deg(m \delta - g_0 b) - \deg(a)$$

$$= \deg(ms - g_0 b) - n$$

$$\deg(g_0) \leq n-1 \quad \text{and} \quad \deg(b) \leq n-1 \\ \Rightarrow \deg(g_0 b) \leq 2n-2$$

$$\deg(m) \leq n-1 \quad \text{and} \quad \deg(s) = n$$

$$\Rightarrow \deg(ms) \leq 2n-1$$

$$\text{Thus} \quad \deg(ms - g_0 b) \leq 2n-1$$

$$\text{Hence} \quad \deg(f_0) \leq n-1 \quad \checkmark$$

$$< n = \deg(s)$$

$$\text{Further} \quad \deg(g_0) < \deg(a) = n = \deg(s)$$

$$\text{Thus} \quad \frac{f_0}{s} \triangleq M \quad \text{and} \quad \frac{g_0}{s} \triangleq N \quad \text{are}$$

both rational, strict, proper.  $\square$

We have thus shown that there is an algorithm to produce desired

$$G_c = \frac{b}{a+m} \quad \text{in} \quad \underline{\text{three distinct steps}}$$

## Compensator Design by Bezout

(1) solve BEZOUT using repeated Euclidean division to obtain  $r_{p-1} = \text{g.c.d.}(a, b) \equiv 1$  and back-substitution.

(2) select  $s$  monic,  $\deg(s) = n$  and define  $f = x^m s$ ;  
 $g = y^m s$ .

(3)  $\hookrightarrow$  Divide  $g$  by  $a$

$$g = l a + g_0$$

$$\deg(g_0) < \deg(a) = n$$

define

$$f_0 = f + l b$$

define

$$M = \frac{f_0}{s} ; N = \frac{g_0}{s}$$

(4) STOP



In practice we would specify

(or get a specification from a customer)

that  $m(s)$  with  $\deg(m) \leq n-1$   
be such that

$a(s) + m(s)$   
has all its roots in desired  
locations in  $\mathbb{C}^-$ .

and

we would choose  $\delta(s)$  monic  
of  $\deg = n$  such that all roots  
of  $\delta$  are in desired locations  
in  $\mathbb{C}^-$ ; this determines how  
fast the observer estimates the  
state

## Example

$$G(s) = \frac{b(s)}{a(s)} = \frac{s+2}{s^3+3}$$

$$\begin{aligned} 1. (i) \quad (s^3+3) &= s^2(s+2) + (-2s^2+3) \\ &\quad \uparrow \\ &\quad a \\ &= s^2(s+2) + (-2s)(s+2) \\ &\quad \quad \quad + 4s+3 \\ &= s^2(s+2) + (-2s)(s+2) \\ &\quad \quad \quad + 4(s+2) - 5 \\ &= (s^2 - 2s + 4)(s+2) - 5 \\ &\quad \quad \quad \uparrow \quad \quad \quad \uparrow \quad \quad \quad \uparrow \\ &\quad \quad \quad q_1 \quad \quad \quad b \quad \quad \quad r_1 \end{aligned}$$

$$\begin{aligned} (ii) \quad (s+2) &= \left(-\frac{2}{5} - \frac{1}{5}s\right)(s+2) + 0 \\ &\quad \uparrow \quad \quad \quad \uparrow \quad \quad \quad \uparrow \quad \quad \quad \uparrow \\ &\quad \quad b \quad \quad \quad q_2 \quad \quad \quad r_1 \quad \quad \quad r_2 \end{aligned}$$

Thus  $r_{p-1} = r_1 = -5$

$$r_1 = a - q_1 b$$

$$-5 = (1)(s^3+3) + (-s^2+2s-4)(s+2)$$

$$\Rightarrow 1 = \left(-\frac{1}{5}\right)(s^3+3) + \left(\frac{s^2}{5} - \frac{2}{5}s + \frac{4}{5}\right)(s+2)$$

$$= x(s) a(s) + y(s) b(s)$$

$$\left. \begin{aligned} \text{Thus } x(s) &= -\frac{1}{5} \\ y(s) &= \frac{s^2}{5} - \frac{2s}{5} + \frac{4}{5} \end{aligned} \right\}$$

2. Suppose we want (or the customer wants) the closed loop characteristic polynomial to be

$$\begin{aligned} p(s) &= a(s) + m(s) \\ &= (s+1)^3 \\ &= s^3 + 3s^2 + 3s + 1 \end{aligned}$$

$$\text{Then } m(s) = 3s^2 + 3s - 2$$

Now select  $\delta(s)$  monic  $\deg(\delta) = 3$

→ We choose  $\delta(s) = s^3 + 3$

$$\text{Then } f = x m \delta = \left(-\frac{1}{5}\right) (3s^2 + 3s - 2) (s^3 + 3)$$

$$g = y m \delta = \left(\frac{s^2}{5} - \frac{2s}{5} + \frac{4}{5}\right) (3s^2 + 3s - 2) (s^3 + 3)$$

3.  $g = l a + g_0$

But  $a$  divides  $g$  exactly since  $\delta = a = s^3 + 3$   
 So  $g_0 = 0 \Rightarrow f_0 = f + l b$

(22)

$$\begin{aligned}
 &= \overbrace{\left(-\frac{1}{5}\right) (3s^2 + 3s - 2) (s^3 + 3)}^f \\
 &\quad + \underbrace{\left(\frac{s^2}{5} - \frac{2}{5}s + \frac{4}{5}\right) (3s^2 + 3s - 2)}_l \underbrace{(s+2)}_b
 \end{aligned}$$

~~$\frac{3s^2 + 3s - 2}{5} (s+2)$~~

$$F = \frac{1}{5} (3s^2 + 3s - 2) \left\{ \begin{array}{l} (s^2 - 2s + 4)(s+2) \\ -(s^3 + 3) \end{array} \right\}$$

$$= \frac{1}{5} (3s^2 + 3s - 2) \left( \begin{array}{l} s^3 - 2s^2 + 4s + 2s^2 - 4s + 8 \\ -s^3 - 3 \end{array} \right)$$

$$= \frac{1}{5} (3s^2 + 3s - 2) (\cancel{s^3} + 5)$$

$$= 3s^2 + 3s - 2$$

$$\text{Thus } M = \frac{f_0}{s} = \frac{3s^2 + 3s - 2}{s^3 + 3}$$

$$N = \frac{g_0}{s} = 0$$

